

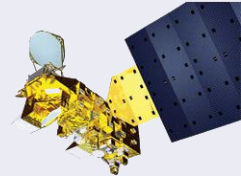
# Radiometric Accuracy Improvements for Version 7

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June 27, 2017

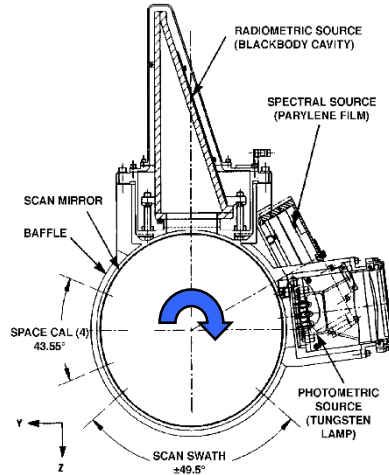
**Preliminary**

# AIRS Designed for High Spectroradiometric Resolution, Accuracy and Stability



## AIRS Features

- Orbit: 705 km, 1:30pm, Sun Synch
- Pupil Imaging IFOV :  $1.1^\circ \times 0.6^\circ$  (13.5 km x 7.4 km)
- Scanner Rotates about Optical Axis (Constant AOI on Mirror)
- Full Aperture OBC Blackbody,  $\epsilon > 0.998$
- Full Aperture Space View
- Solid State Grating Spectrometer
- Temperature Controlled Spectrometer: 158K
- Actively Cooled FPAs: 60K
- No. Channels: 2378 IR, 4 Vis/NIR
- Mass: 177Kg,  
Power: 256 Watts,  
Life: 5 years (7 years goal)

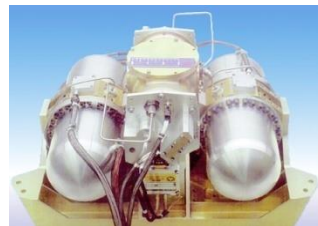


## Isolated Scan Cavity



## Grating Spectrometer

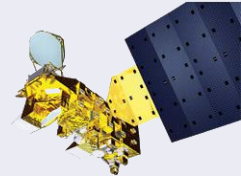
IR Spectral Range:  
3.74-4.61  $\mu\text{m}$ , 6.2-8.22  $\mu\text{m}$ ,  
8.8-15.4  $\mu\text{m}$   
IR Spectral Resolution:  
 $\approx 1200 (\lambda/\Delta\lambda)$   
No. IR Channels: 2378 IR



## Active Detector Cooling

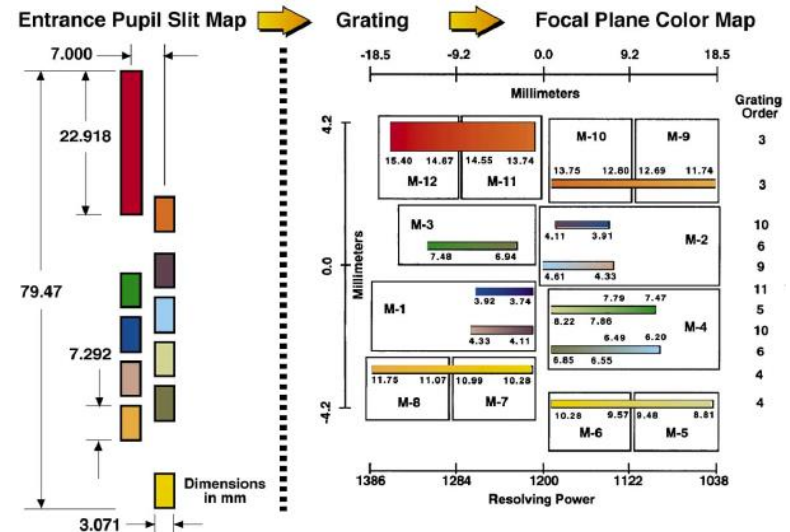
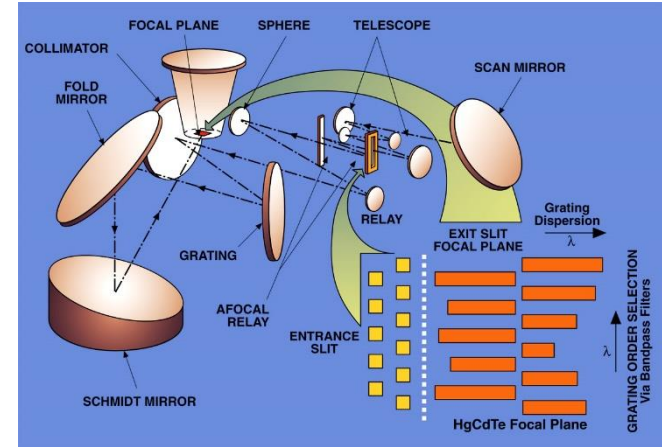
## Temperature Controlled Instrument

# AIRS Spectral Bands Defined by 11 Entrance Apertures and 17 Detector/Filter Modules

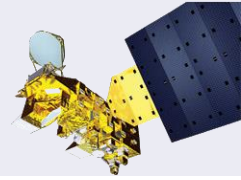


AIRS Module Spectral Band Limits

		$\lambda_1$	$\lambda_2$	$\nu_1$	$\nu_2$
		( $\mu\text{m}$ )	( $\mu\text{m}$ )	( $\text{cm}^{-1}$ )	( $\text{cm}^{-1}$ )
1	M1a	3.752	3.934	2541.9	2665.2
2	M1b	4.127	4.348	2299.8	2422.8
3	M2a	3.891	4.088	2446.2	2569.8
4	M2b	4.301	4.584	2181.5	2325.0
5	M3	6.930	7.473	1338.2	1443.1
6	M4a	6.196	6.489	1541.1	1613.9
7	M4b	6.549	6.848	1460.3	1527.0
8	M4c	7.469	7.786	1284.3	1338.9
9	M4d	7.858	8.217	1217.0	1272.6
10	M5	8.798	9.469	1056.1	1136.6
11	M6	9.558	10.269	973.8	1046.2
12	M7	10.264	10.974	911.2	974.3
13	M8	11.065	11.744	851.5	903.8
14	M9	11.731	12.670	789.3	852.4
15	M10	12.790	13.735	728.1	781.9
16	M11	13.728	14.543	687.6	728.4
17	M12	14.663	15.394	649.6	682.0



# AIRS Radiometric Transfer Equations Used to Identify Error Terms



## Radiometric Transfer Equations

$$N_{sc,i,j} = \frac{a_o(\theta_j) + a_{1,i}(dn_{i,j} - dn_{sv,i}) + a_2(dn_{i,j} - dn_{sv,i})^2}{1 + p_r p_t \cos 2(\theta_j - \delta)}$$

$$a_o(\theta_j) = P_{sm} p_r p_t [\cos 2(\theta_j - \delta) + \cos 2\delta]$$

$$a_{1,i} = \frac{N_{OBC,i}(1 + p_r p_t \cos 2\delta) - a_o(\theta_{OBC}) - a_2(dn_{obc,i} - dn_{sv,i})^2}{(dn_{obc,i} - dn_{sv,i})}$$

$N_{sc,i,j}$  = Scene Radiance ( $\text{mW}/\text{m}^2\text{-sr}\text{-cm}^{-1}$ )

$P_{sm}$  = Planck radiation function

$N_{OBC,i}$  = Radiance of the On-Board Calibrator Blackbody

$i$  = Scan Index,  $j$  = Footprint Index

$\theta$  = Scan Angle.  $\theta = 0$  is nadir.

$dn_{i,j}$  = Raw Digital Number in the Earth View

$dn_{sv,i}$  = Space view counts offset.

$a_o$  = Radiometric offset.  $a_{1,i}$  = Radiometric gain.

$a_2$  = Nonlinearity

$p_r p_t$  = Polarization Factor Product

$d$  = Phase of the polarization

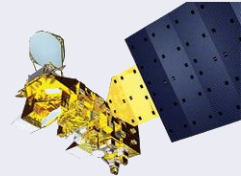
## Radiometric Accuracy Equation

$$\partial N_{sc}^2 = \left( \frac{\partial N_{sc}}{\partial p_r p_t} \Delta p_r p_t \right)^2 + \left( \frac{\partial N_{sc}}{\partial \delta} \Delta \delta \right)^2 + \left( \frac{\partial N_{sc}}{\partial T_{sm}} \Delta T_{sm} \right)^2 + \left( \frac{\partial N_{sc}}{\partial \theta} \Delta \theta \right)^2 + \left( \frac{\partial N_{sc}}{\partial \varepsilon_{OBC}} \Delta \varepsilon_{OBC} \right)^2 + \left( \frac{\partial N_{sc}}{\partial T_{OBC}} \Delta T_{OBC} \right)^2 + \left( \frac{\partial N_{sc}}{\partial a_2} \Delta a_2 \right)^2 + \left( \frac{\partial N_{sc}}{\partial dn} \Delta dn \right)^2$$

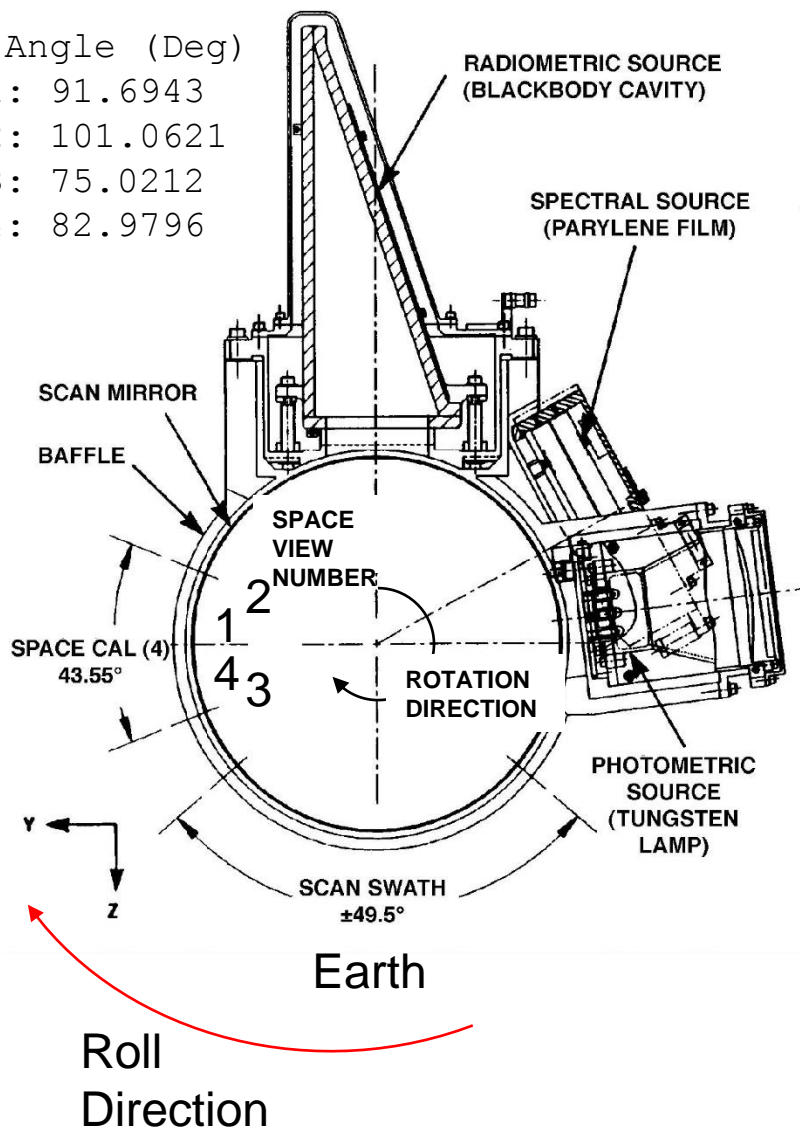
T. Pagano et al., "Pre-Launch and In-flight Radiometric Calibration of the Atmospheric Infrared Sounder (AIRS)," IEEE TGRS, Volume 41, No. 2, February 2003, p. 265

T. Pagano, H. Aumann, K. Overoye, "Level 1B Products from the Atmospheric Infrared Sounder (AIRS) on the EOS Aqua Spacecraft", Proc. ITOVS, October 2003

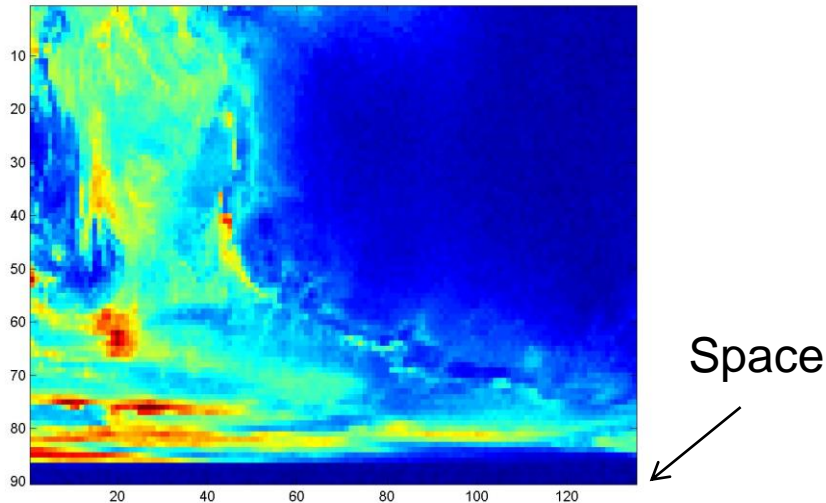
# 4 Spaceviews Enable Calibration of Mirror Polarization. Roll provides Validation.



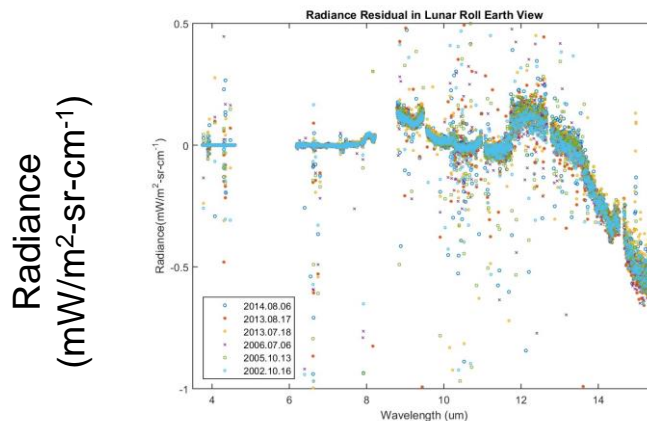
SV Angle (Deg)  
 SV1: 91.6943  
 SV2: 101.0621  
 SV3: 75.0212  
 SV4: 82.9796



BT Ch 2333, 2616  $\text{cm}^{-1}$



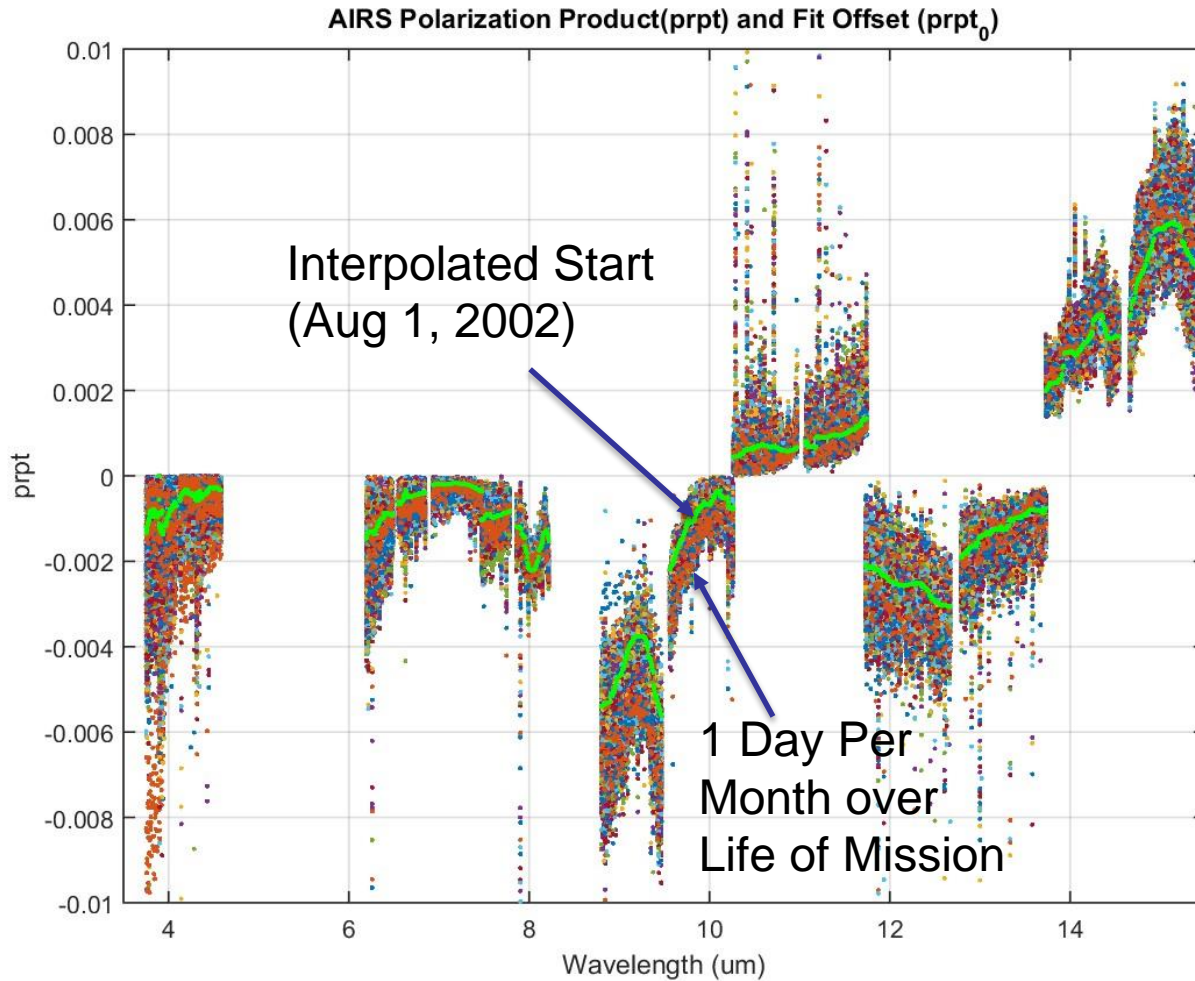
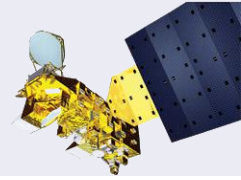
Earth View - Space View Radiance



$$(dn_x - dn_{s1})a_1 = -P_{sm}p_r p_t [\cos 2\delta \cos 2\theta_x + \sin 2\delta \sin 2\theta_x + \cos 2\delta] \quad 5$$

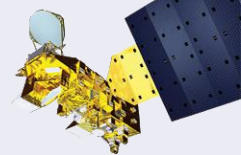


# Polarization and Phase Derived from SV Data over Entire Mission

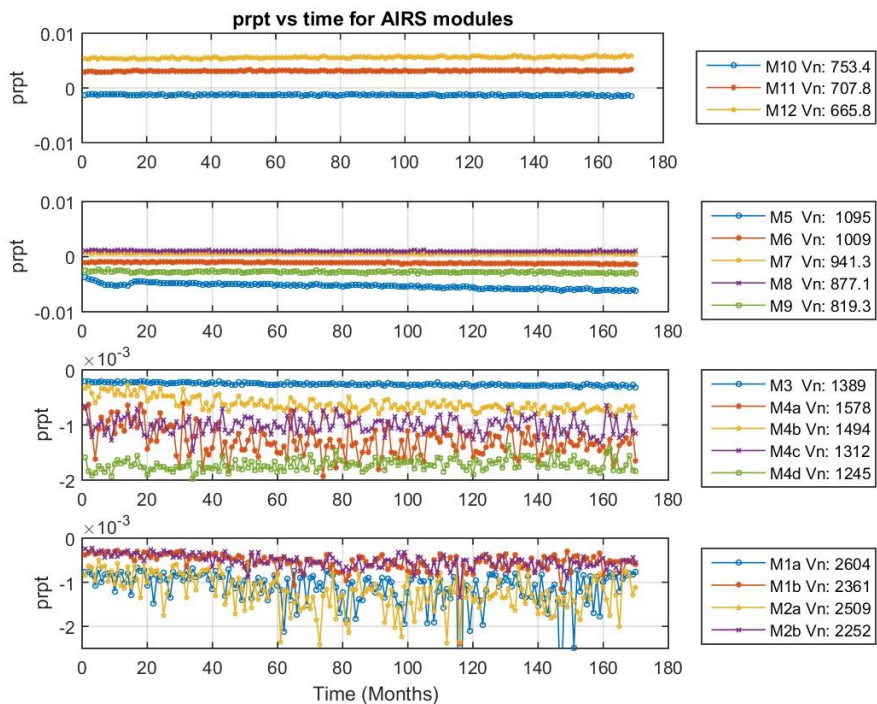


Preliminary

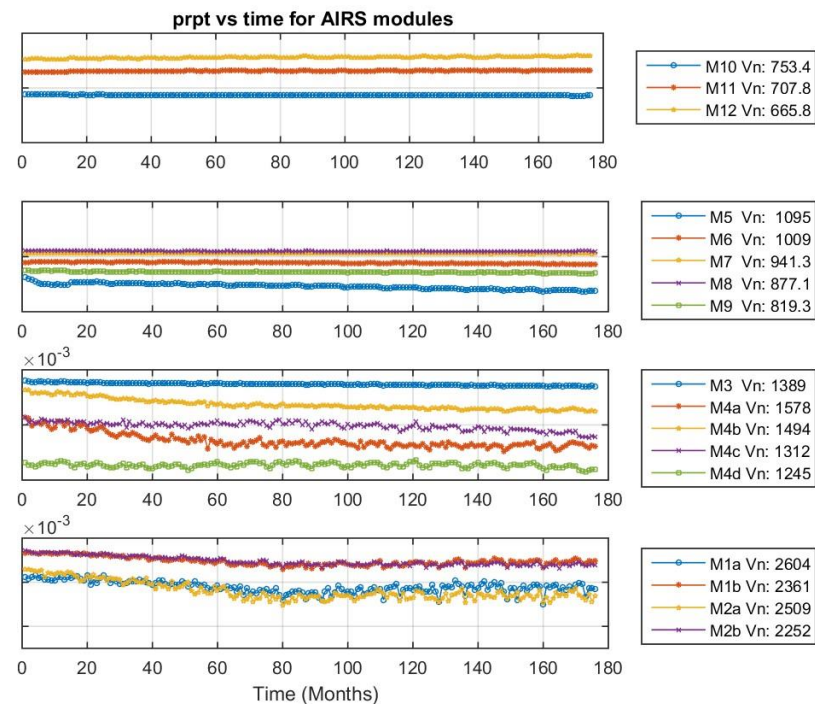
# 30d Average Improves In-orbit Characterization of AIRS Mirror Polarization Trends



## One Day Per Month

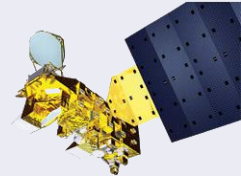


## 30d Average Day Per Month

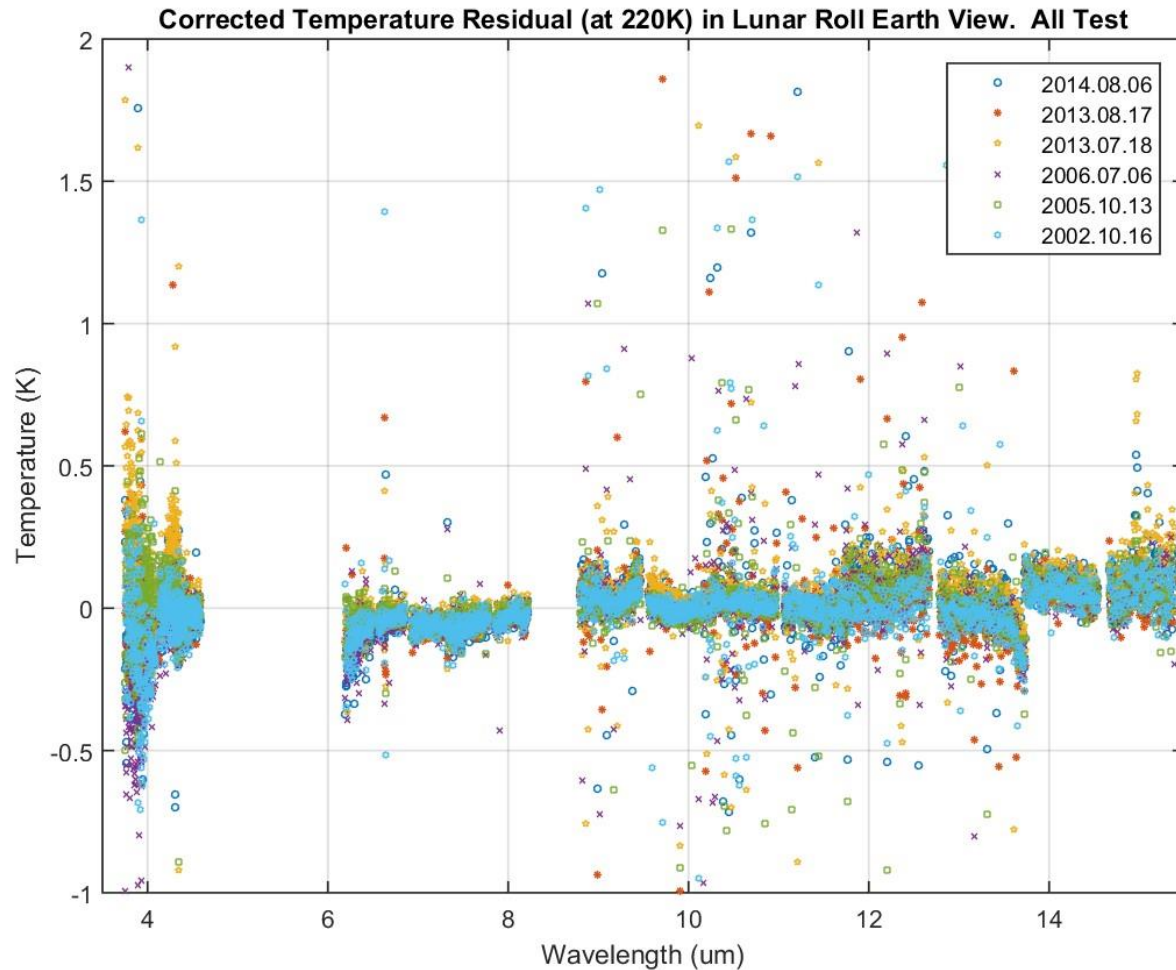


Preliminary

# Coefficients derived from space views applied to roll test produce low errors



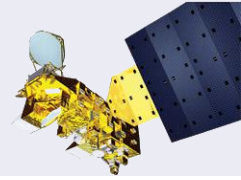
Derived radiance in Earth Viewport of deep space (spacecraft roll maneuver) expressed in terms of temperature at 220K



Preliminary

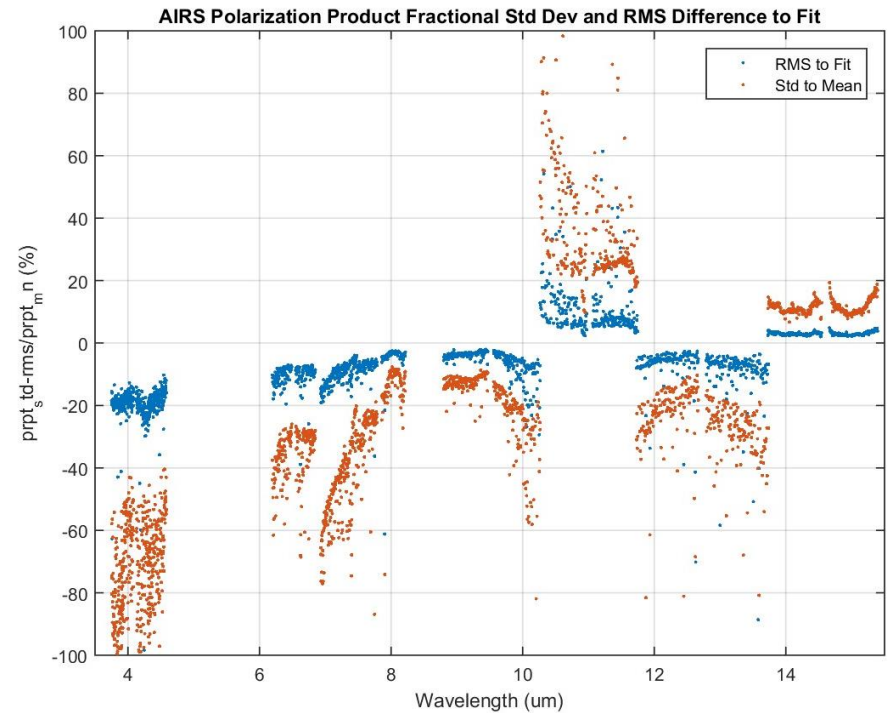
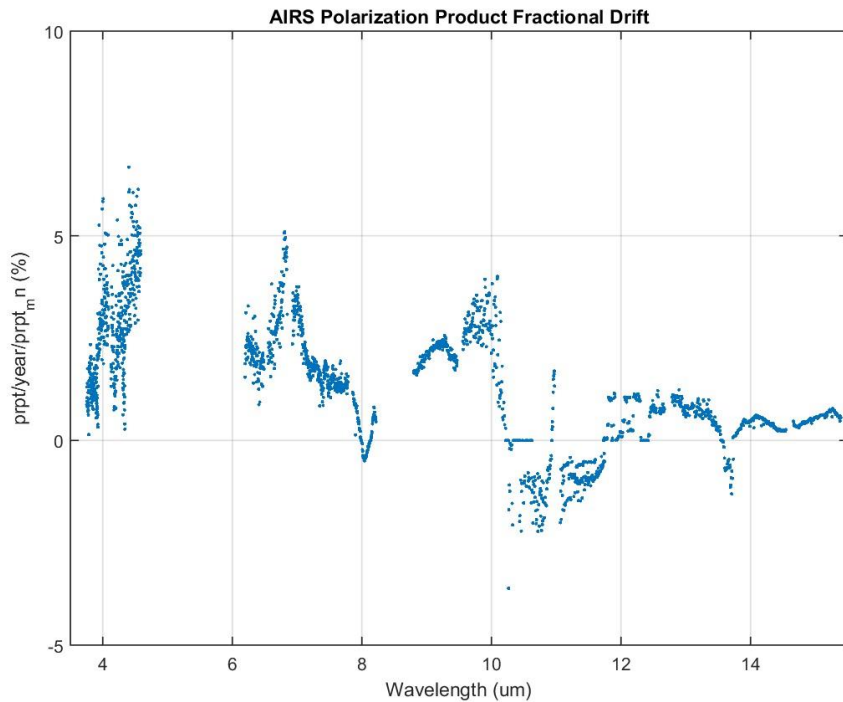


# Linear fit gives annual trend. Time dependent polarization reduces errors.



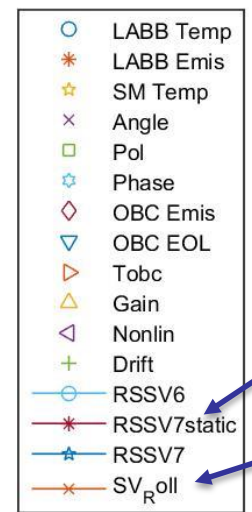
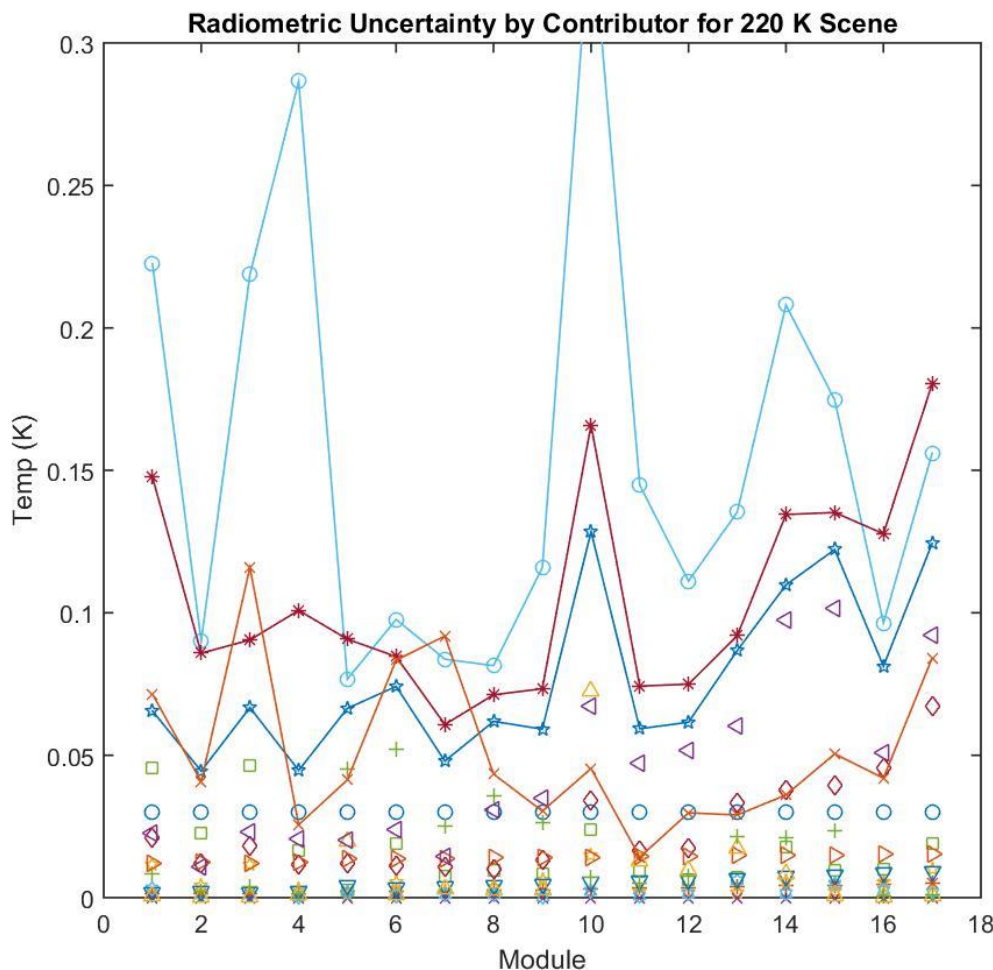
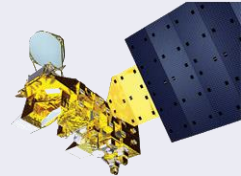
Trend in polarization is up to 5% of nominal per year

Time dependent polarization fit (blue) reduces errors compared to static (red)



Preliminary

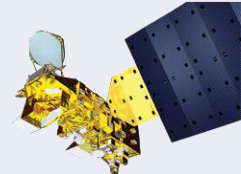
# Contributors to radiometric error at 220K and totals compared to prior versions



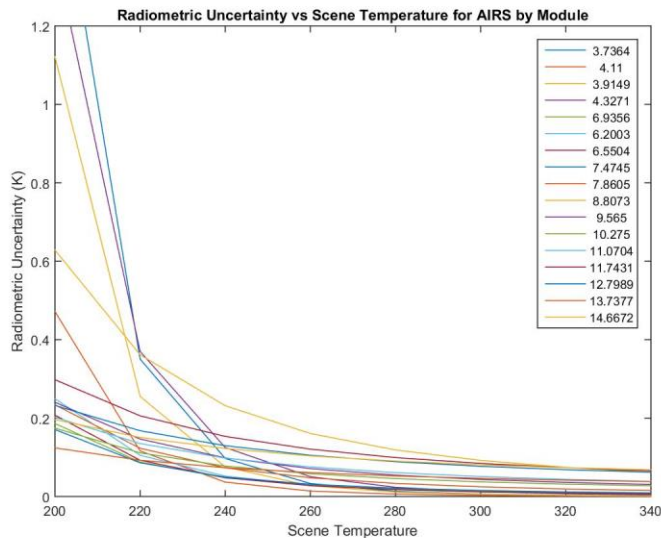
- Improvement in accuracy of more recent versions attributed to better polarization amplitude and phase estimates
- V7 coefficients applied to space view roll

Preliminary

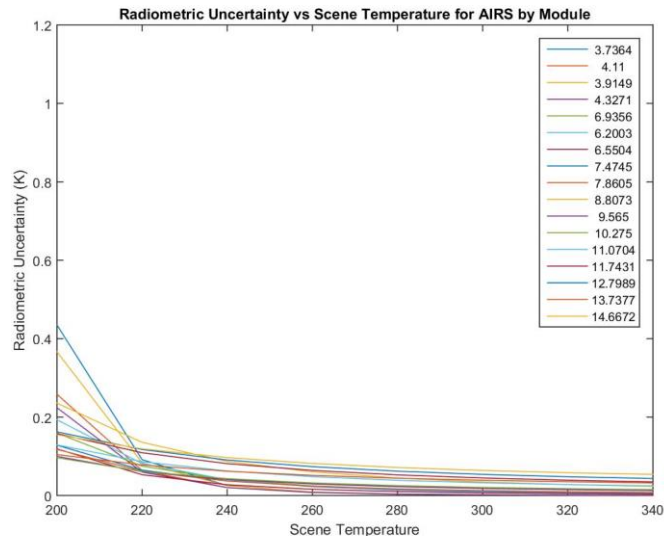
# Radiometric accuracy expected to be better for low scene temperatures in Version 7



v6

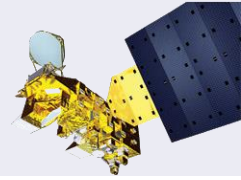


v7



V7	AIRS Module	$\lambda_1(\mu\text{m})$	T(K) 200	T(K) 220	T(K) 240	T(K) 260	T(K) 280	T(K) 300	T(K) 320	T(K) 340
1	M1a	3.752	0.435	0.091	0.025	0.009	0.003	0.002	0.001	0.000
2	M1b	4.127	0.258	0.064	0.020	0.008	0.003	0.002	0.001	0.001
3	M2a	3.891	0.367	0.083	0.025	0.009	0.004	0.002	0.001	0.001
4	M2b	4.301	0.224	0.060	0.020	0.008	0.004	0.002	0.001	0.001
5	M3	6.930	0.159	0.075	0.041	0.025	0.016	0.011	0.008	0.006
6	M4a	6.196	0.193	0.081	0.040	0.022	0.014	0.009	0.006	0.005
7	M4b	6.549	0.119	0.053	0.027	0.016	0.010	0.007	0.005	0.004
8	M4c	7.469	0.128	0.065	0.037	0.024	0.016	0.012	0.009	0.007
9	M4d	7.858	0.118	0.062	0.037	0.024	0.017	0.012	0.010	0.008
10	M5	8.798	0.236	0.136	0.087	0.060	0.045	0.035	0.028	0.023
11	M6	9.558	0.100	0.061	0.041	0.030	0.023	0.018	0.015	0.013
12	M7	10.264	0.096	0.062	0.043	0.032	0.025	0.021	0.017	0.015
13	M8	11.065	0.129	0.086	0.063	0.048	0.039	0.033	0.028	0.025
14	M9	11.731	0.158	0.109	0.081	0.064	0.053	0.045	0.039	0.035
15	M10	12.790	0.162	0.117	0.091	0.074	0.062	0.054	0.048	0.043
16	M11	13.728	0.104	0.078	0.062	0.051	0.044	0.039	0.035	0.032
17	M12	14.663	0.155	0.119	0.091	0.082	0.071	0.064	0.058	0.054

Preliminary



- AIRS radiometric accuracy at low temperatures driven by knowledge of the mirror polarized emission ( $p_r p_t$  and  $\delta$ )
- View of space during normal scanning operations enables in-flight derivation of polarized emission
- Terms applied to earth view during spacecraft roll show low residual errors
- Significant improvement over v6 errors
- Worst problem (biggest improvement) at short wavelengths and cold temperatures.
- Next Steps:
  - Test: Examine sample and ACDS data sets compared to prior versions
  - Validate:
    - Check trends on Deep Convective Clouds
    - Revisit validation of polar regions
  - Cross-compare
    - Compare with IASI and CrIS